

Deformation Modelling in Interreg 4A project IRFO - Intelligent Robots for Handling of Flexible Objects

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Deformation
Modelling

Fugl

Outline

Modelling

Elasticity

Introduction

Hooke's Law

Stress tensor

Strain tensor

Stiffness tensor

Equations of motion

Experiences

Present work

Summary



Outline

- 1** The need for Modelling
- 2** Modelling in context of IRFO system
- 3** Behaviour of Flexible Objects
- 4** Accomplished
- 5** Future plans

The need for Modelling

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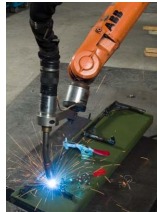
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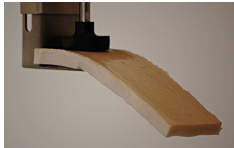
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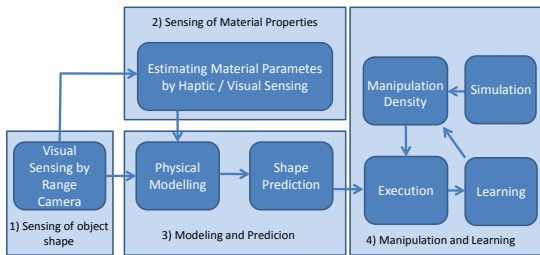
Rigid: Idealization, neglecting deformation

- The assumption of traditional robotics
- Keeps mathematical models simple.
- No such thing as a rigid object!
- An physical approximation for stiff



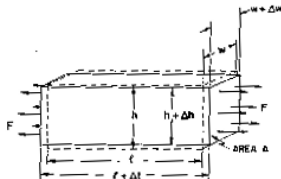
When is something elastic?

- Always! - but rigid may be a very good approximation
- Relevant parameters
 - Scale
 - Forces
 - Length
 - Stiffness
 - Weight



Modelling and Prediction

- Receives object shape data from stage 1) and material properties from stage 2)
- Predicts the shape and sends data to the Manipulation/Learning stage



Relating stress and strain

- $\frac{F}{A} = E \times \frac{\Delta l}{l}$
- **Stress** - force per unit area $\frac{F}{A}$
- Young's modulus E
- **Strain** - stretch per unit length $\frac{\Delta l}{l}$

What's going to happen

- We're making **Hooke's Law**
 $\text{Stress} = (\text{Youngs Modulus}) \times (\text{Strain})$ work on a 3D elastic body for all sorts of crazy deformations, then we combine it with **Newton's 2nd Law** and end up with equations of motion
- In place of the simple stress (force) in Hooke's Law we're going to introduce **the stress tensor**, and in place of the simple strain (deformation) we're introducing **the strain tensor**

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Generalizing Hooke's Law

- *Stresses are proportional to the strains*
- We must linearly relate each component of the stress tensor σ_{kl} to each component of the strain tensor u_{ik}

$$\sigma_{ij} = \sum_{k,l} C_{ijkl} u_{kl}$$

- where C_{ijkl} is the **stiffness tensor**
- Multi-dimensional analog to spring constant ($F = -kx$)

The equations of motion for an elastic material

- We skipped a few steps, where we revisited Newton's 2nd Law and our vector calculus
- For the important special case of a *homogeneous, isotropic* material we end up with

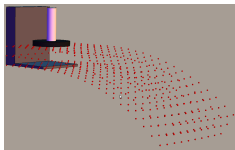
$$\rho \frac{\partial^2 \mathbf{u}}{\partial t^2} = (\lambda + \mu) \nabla(\nabla \cdot \mathbf{u}) + \mu \nabla^2 \mathbf{u} \quad (3)$$

- where λ and μ are the Lamé coefficients
- This PDE is the Navier-Cauchy equation

3D numerical solution to Navier-Cauchy PDE

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$$\begin{aligned}
 f_x = (\lambda + \mu) & \left[\frac{u_x(i+1, j, k) - 2u_x(i, j, k) + u_x(i-1, j, k)}{h_x^2} \right. \\
 & + \frac{u_y(i+1, j+1, k) - u_y(i+1, j-1, k) - u_y(i-1, j+1, k) + u_y(i-1, j-1, k)}{4h_x h_y} \\
 & \left. + \frac{u_z(i+1, j, k+1) - u_z(i+1, j, k-1) - u_z(i-1, j, k+1) + u_z(i-1, j, k-1)}{4h_x h_z} \right] \\
 & + \mu \left[\frac{u_x(i+1, j, k) - 2u_x(i, j, k) + u_x(i-1, j, k)}{h_x^2} \right. \\
 & + \frac{u_x(i, j+1, k) - 2u_x(i, j, k) + u_x(i, j-1, k)}{h_y^2} \\
 & \left. + \frac{u_x(i, j, k+1) - 2u_x(i, j, k) + u_x(i, j, k-1)}{h_z^2} \right]
 \end{aligned}$$

Finite Difference Simulation software developed

- *An Outline for an intelligent System performing Peg-in-Hole Actions with flexible Objects, ICIRA 2011*
- + Supports relevant robotics grasping situations
- + Full 3D deformation output
- - Computationally expensive (seconds per frame), but large room for optimization, GPUs, etc.
- -Domain problems!

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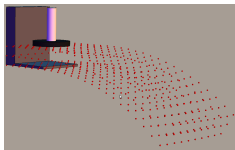
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$$f_x = (\lambda + \mu) \left[\frac{u_x(i+1, j, k) - 2u_x(i, j, k) + u_x(i-1, j, k)}{h_x^2} + \frac{u_y(i+1, j+1, k) - u_y(i+1, j-1, k) - u_y(i-1, j+1, k) + u_y(i-1, j-1, k)}{4h_x h_y} + \frac{u_z(i+1, j, k+1) - u_z(i+1, j, k-1) - u_z(i-1, j, k+1) + u_z(i-1, j, k-1)}{4h_x h_z} \right] + \mu \left[\frac{u_x(i+1, j, k) - 2u_x(i, j, k) + u_x(i-1, j, k)}{h_x^2} + \frac{u_x(i, j+1, k) - 2u_x(i, j, k) + u_x(i, j-1, k)}{h_y^2} + \frac{u_x(i, j, k+1) - 2u_x(i, j, k) + u_x(i, j, k-1)}{h_z^2} \right]$$

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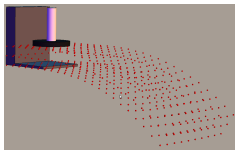
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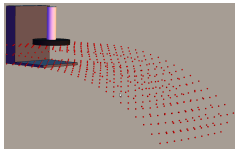
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3D numerical instability

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 & \left. \left. + \frac{u_x(i, j, k+1) - 2u_x(i, j, k) + u_x(i, j, k-1)}{h_z^2} \right] \right]
 \end{aligned}$$

Domain

- Experiences: Soft materials + thin object = large strains/rotations: **Numerical instability**
- Stable up to deformation angles of around 30° - Not sufficient for IRFO!
- Root cause: Linearizing simplification in theory (strain tensor)

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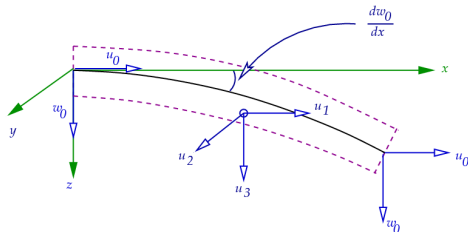
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Beam models

- Bending deformation only
- Stretching in x -direction neglected
- Cross-section info (y and z) through second moment of inertia I .

$$EI \frac{d^4 w}{dx^4} = q(x) \quad (4)$$

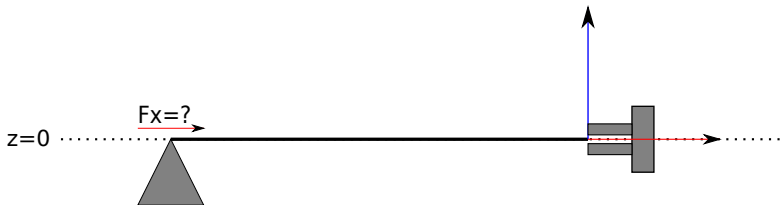
Small deformation

- *Learning Peg-In-Hole Actions with flexible Objects, SSIR 2012*
- Same linear strain tensor as Navier-Cauchy PDE, but has analytical solutions which are inherently stable
- Geometric post-processing can compensate for these errors.

$$EI \frac{d^4 w}{dx^4} - \frac{3}{2} EA \left(\frac{dw}{dx} \right)^2 \left(\frac{d^2 w}{dx^2} \right) = q(x) \quad (5)$$

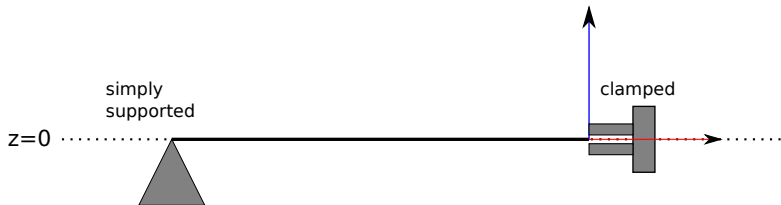
Large-deformation

- Here shown for constant E , I and A
- Extra **non-linear term** (second order effects included)
- Numerical solution methods the only viable option



■ The problem:

- **Laying down/Placement operation**
- Determine the unknown elastic force $F_x(x=0, t)$ due to bending, at the table contact point.
- Point is fixed due to static friction, but for some critical force F_{crit} it will begin to slide.

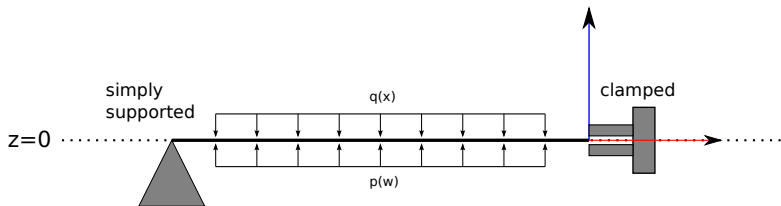


■ Assumptions:

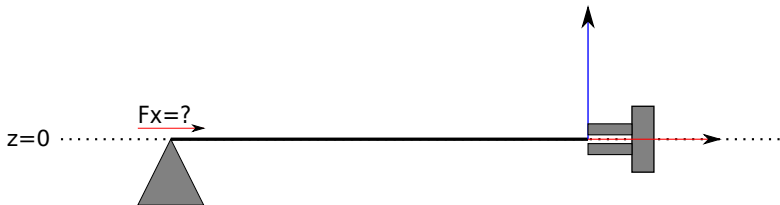
- End at $x = 0$ is fixed on the table, but free to rotate
- End at $x = L$ is grasped by the robot gripper, with a known position and rotation

■ Boundary conditions:

- $x=0$: Simply supported, $w(0, t) = 0$, $w''(0, t) = 0$
- $x=L$: Clamped: $w(L, t) = f(t)$, $w'(L, t) = g(t)$



- Penalize table contact ($w < 0$):
 - $p(w) = F_p H(0 > w > -\varepsilon)$
 - $H(w)$ is the Heaviside step function
 - F_p is the penalty force
- Include as an extra source term:
 - E.g. $EI \frac{d^4 w}{dx^4} + \dots = q(x) + p(w)$
 - If not already, equation will become non-linear



- Having solved for the deformation $w(x, t)$ by the constitutive laws of elasticity, strain and geometric relations we obtain $F_x(x = 0, t)$.
- Should $F_x(x = 0, t)$ exceed some critical limit F_{crit} , the object will overcome static friction and begin to slide



- Grasping
 - *An Outline for an intelligent System performing Peg-in-Hole Actions with flexible Objects, ICIRA 2011*
- Peg-in-Hole
 - *Learning Peg-In-Hole Actions with flexible Objects, SSIR 2012*
- Placement/Laying down operations (Modelling and Learning)
 - Ongoing work, as presented
- Vision integration and estimation of parameters
 - Ongoing work



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Thanks for your attention